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REFLECTION FOR SEVERAL STANDARD SURFACE MATERIALS

Quarterly Progress Report, Part 2

Contract No. AF 33 (657)-9014

1 October 1962 — 31 December 1962

Prepared by:

Dr. Werner Rambauske Ronald Hodge

University of Dayton

Research Institute

Dayton 9, Ohio



Prepared for:

Aeronautical Systems Division

Air Force Systems Command

Reconnaissance Laboratory

Wright Patterson Air Force Base, Ohio

DEVIATION FROM LAMBERTIAN OPTICAL REFLECTION FOR SEVERAL STANDARD SURFACE MATERIALS

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HEADQUARTERS

Aeronautical Systems Division

AIR FORCE SYSTEMS COMMAND UNITED STATES AIR FORCE WRIGHT-PATTERSON AIR FORCE BASE, OHIO

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FOR THE COMMANDER

LEOLIN E. LONG

Chief. Optronics Branch Reconnaissance Division Atch

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NOMENCLATURE

i	Angle of Incidence Measured Between the Light from the Collimator and the Normal to the Sample Surface.
r	Angle of Reflection Measured Between the Reflected Light Received by the Telescope and the Normal to the Sample Surface
Ii	Current Reading on the Electrometer Corresponding to the Incident Light Flux (Plus the Background) Weighted by the Sensitivity of the Photomultiplier Plus Dark Current
Ir	Current Reading on the Electrometer Corresponding to the Reflected Light Flux from the Sample in a Cone of 10 Arcminutes Plus the Background Weighted by the Sensitivity of the Photomultiplier Plus Dark Current.
ľį	${f I_i}$ Adjusted for Background, Dark Current, Lamp Voltage and Reference.
I'r	$I_{ extbf{T}}$ Adjusted for Background, Dark Current, Lamp Voltage and Reference.
b.c.	Current Reading with Room Lights Off, Light from the Collimator Closed Off and Telescope Open.
d.c.	Dark Current of Photomultiplier (d.c. = b.c.)
B.G.	Total Background, equal to b.c. Plus Background Off Sample Support (with Disc Removed) with Light from the Collimator Present.
ref.	Reference
t	Thickness of Sample Coating.
2 r	Diameter of Sample.
Wr #	Wratten Filter Number.
ND #	Neutral Density Number Optics Technology Filters.
Mg0 #3	Disc Sample Coated with MgO (t=2,0mm)
W.P. #1	First White Paint Sample Coating,

QUARTERLY PROGRESS REPORT

Contract AF 33(657)-9014

1 October 1962 - 31 December 1962

1. INTRODUCTION

This is Part 2 of the second Quarterly Progress Report submitted in partial fulfillment of the requirements of Contract AF 33(657)-9014. The report covers a phase of the work completed during the period 1 October 1962 through 31 December 1962, and is concerned with the experimental determination of the degree of departure from Lambertian optical reflection for several standard surface materials.

2. WORK PERFORMED

In conjunction with the determination of optical cross-sections of various geometrical bodies, this report is concerned with the investigation of the departure from Lambertian optical reflection for several standard surface materials under different angles of incidence. As the measurements of the near horizontal reflecting power which were made for standard geometrical bodies and models of actual targets did show discrepancies with values calculated according to simple laws of reflection, a more thorough investigation of the actual prevailing relations was indicated. If one wants to perform integrations over various surface shapes in order to find an estimated value for the reflected power, one usually assumes complete diffusion according to Lambert's law. However, in every case of a material used for the surface of an actual target very substantial deviations from complete diffusion can exist and sometimes even specular reflection may occur.

Although investigations and measurements about these problems have been done in the past, they are not applicable for specific optical radar and photometric problems such as detection, recognition, and tracking of artificial targets. The reasons are:

- 1) Measurements are not easily accessible (1870-1920) and were published a long time ago.
- 2) The accuracy of these measurements is not too reliable because visual photometry instead of photoelectric measurements was employed.

- 3) From the almost infinite variety of materials those were investigated which have practically no bearing on modern space and aircraft designs.
- 4) Since problems of this kind were of no great importance in the time when investigated, one cannot derive, because of the scarcity of the data, relationships which are applicable for today's problems of optical cross-sections.

The behavior of reflected coherent light, especially when of narrow band-width and a high degree of polarization as is given in most cases of laser illumination, will be even more particular for specific materials and surface arrangements. Hence it is intended to compare the values given in this report which will serve as standards with those found under the same conditions by laser illumination. Sets of measurements of this kind will then lead to the prediction of the general behavior of certain surface materials and surface forms. Mathematically, these sets of measurements will be approximated by empirical equations which express the reflected power as a function of angle of incidence and some prevalent parameters of material reflection coefficient and body shape factor.

Several diffuse samples were investigated which approach an ideally diffuse surface, and these measurements were compared to measurements of reflections from a special white paint and from polished aluminum. The source of illumination was incandescent incoherent light. The investigation of other materials will be added in the future.

3. EQUIPMENT

The experiments were conducted in the X-Ray Laboratory at the University of Dayton, Dayton, Ohio. In this laboratory the surroundings could be darkened to less than the noise level of the measuring device. Furthermore the photometric system was curtained off in one corner with the electrometer and observer outside while the measurements were being made.

The experiment was set up on a Gaertner L124 high precision spectrometer which had already been aligned to ±1 arc second for previous experimentation and checked with a calibrated prism obtained from the National Bureau of Standards.

A tungsten ribbon filament lamp (G.E. 18A/T10/1) and a condensing lens were sealed into a box at one end of the collimator and ventilated as shown in Figure 1. The ribbon filament was imaged on the entrance aperture of the collimator by the condensing lens and aligned so that a uniform beam of parallel

light was obtained from the collimator. A 6 Vdc, 18 amps, regulated lamp power supply built at the University of Dayton was monitored to *0.01 volts. Filters could be placed immediately in front of the entrance aperture. This aperture was square and its width subtended an angle of 10 arcminutes at the center of the spectrometer the dimensions of which are shown in Figure 1. The sample was mounted on the rotation axis of the spectrometer in the center of the beam of collimated light. (See Figure 2.) Only the sample and part of its supporting shaft were in the beam of incident light. The sample was aligned perpendicular to the incident light by auto-collimating on its back surface which was nearly plane parallel with the front surface. The alignment was checked at the end of a series of measurements. The spectrometer table could be rotated in one plane and angles of incidence i were set with the circular scale attached to the table and could be read to *1 arcminute with a vernier.

Reflected light was observed through the telescope with a photomultiplier fixed to the exit aperture. The photomultiplier used was type 931A (Sylvania Electric Products, Inc.) with an S4 response and an average sensitivity of 30 µamp/lumen for tungsten light. It was powered with N.J.E. Corporation Model S-326 high voltage power supply at 1000 volts dc with a ripple content of only one part in 100,000. Current was detected with a Keithley Model 610A electrometer. The telescope was positioned opposite the collimator, and a stop with a circular aperture of 10 arcminutes subtended from the center of the spectrometer was placed in the focal plane of the telescope (this position was determined with a small error of up to 1 millimeter) and in juxtaposition with the image of the entrance aperture of the collimator. The spectrometer circle was zeroed to read 180° for this position of the telescope. The photomultiplier was securely attached with the cathode surface 3cm behind the focal plane and was not moved from this fixed position throughout a set of measurements.

A black felt cloth backdrop was hung opposite the telescope, and the photomultiplier housing was taped and surrounded with black coth. The spectrometer table was covered with black felt paper, and surfaces near the sample were painted flat black.

Angular setting of the spectrometer and readings on the electrometer were made directly. Temperature and humidity were kept constant at 24°C. * 1°C. and 15% * 5% respectively.

4. MEASUREMENTS

Measurements were made on the following seven samples:

- A front surface mirror, whose surface area was 4.8cm², which was simply stood on edge on the spectrometer table with the lower edge stopped off.
- 2) The same front surface mirror employed as a diffuse sample after it was smoked with MgO to a coating thickness of t=0.5mm.
- 3) Similar to sample #2 except the mirror was smoked with MgO to a coating thickness of t=1.0mm.
- 4) An aluminum disc (2r=2.5cm, A=5.0cm²) smoked with MgO to a coating thickness t=2mm. The aluminum surface was highly polished although the edges were slightly rounded. The rim was covered with black felt paper and the vertical supporting shaft was painted flat black.
- 5) A highly polished and somewhat flatter end of a cylinder (2r=2.5cm) fine sprayed with a special white paint received from Surveillance Branch, Reconnaissance Laboratory, Wright-Patterson Air Force Base, Ohio, to about a two or three coat thickness. The surface appeared very smooth and wet even after it had dried. The side edges of the cylindrical body were painted flat black.
- 6) The same cylinder with a much heavier smooth coat of the same paint.
- 7) The highly polished specular base of a 30° half angle aluminum cone (2r=2.5cm) was measured. Again, the surface, though well polished, was slightly rounded near the edge. The lateral surface of the cone was painted flat black.

The background current (b.c.) given in the data sheets is the photomultiplier readings obtained with room lights off, collimator closed and telescope open to catch stray background reflections. It was equal to the photomultiplier dark current in all instances and therefore indicates that the surroundings were sufficiently darkened.

The background of the black supporting shaft with the collimator open was measured with the sample removed (see Table 6). There is some question about the background for measurements of very large angles (i+r large) due to the secondary reflection from

the front of the collimator and scattered light from its lens. The telescope did not see the illuminated blackened surfaces of the sample except for a few measurements on the negative side. These measurements seemed to be only slightly affected, if at all, by the reflected light from these blackened surfaces.

The background from the shaft at any telescope setting was added to the background current and this sum subtracted from the sample reflection current reading. Improvements in sample mount that will reduce background are shown in Figure 3. The entire equipment area has since been painted flat black.

Adjustments were made in the readings for lamp voltage variation. At $\rm I_T=1.80 \times 10^{-7} amps$ a change in lamp voltage of 0.02 volts resulted in an average change of 0.035 x 10⁻⁷ amps in $\rm I_T$ and this corresponding correction was applied proportionately to each reading.

Measurements of the incident light $I_{\underline{i}}$ were made by replacing the sample as accurately as possible with a stop opening in the same position. Measurements were made at four angles of incidence. Each value was divided by the cosine of the angle of incidence at which it was obtained and these quotients, which were nearly equal, were averaged to obtain the full incident light $I_{\underline{i}}$ at normal incidence (i=0°). Measurements were made both with the stop in the focal plane of the telescope in place and with this stop removed. In this way it should be possible to detect any uncollimated light in the incident beam since this uncollimated light would be focused by the telescope outside the image of the entrance aperture. Very little uncollimated light was observed in the incident beam visually and so a value for the incident light ($I_{\underline{i}}$) was taken for measurements with the stop in the telescope removed.

Specular reflections from white paint and aluminum were measured with the stop in the focal plane of the telescope. Since angles of incidence could only be set with a precision of 2 arcminutes on the graduated circle attached to the spectrometer table, measurements of specular reflections were made by varying the telescope position slightly and observing maximum readings. In measuring the specular reflections off the special white paint not all of the specular reflection was received through the exit aperture because the surface of the white paint only approximates a pure specular surface. Therefore the reflected light measurements represent the total light flux emitted from the sample in a cone of 10 arcminutes.

Measurements of incident light (I_1) and specular reflections had to be taken using ND filters. The transmission of these filters was measured separately but because of the limited range of the photomultiplier it was not possible to measure them in combination at this time. This measurement was needed for

determining I_1 . A nominal value of 10^{-6} was therefore taken for the transmission of ND #2; #3, and #1 in combination. However, this value is sufficient for presenting the information which is of interest now.

Measurements were made with white light of tungsten at 5.00 volts and with Optics Technology interference filters #436, #546, and #656 with a band pass as shown in Figures 4, 5 and 6. These measurements of the reflected light are dependent upon the sensitivity of the photomultiplier as a function of wavelength, and when the photomultiplier is calibrated it will be possible to take into consideration the selective reflection of these samples. Measurements were made for i=0°, 20°, 40°, 60°, 80° and r was varied in 10° steps and in one degree steps around points of interest such as i=r, the surface normal and at large angles greater than 85°.

After the preliminary measurements on the first few samples, all data for the diffuse reflection for the MgO coated disc and samples coated with white paint were normalized in the following way. For each set of measurements at an angle of incidence (i) a reference measurement at i=0°, r=45° was made. Ratios were taken of the reference measurements off MgO and also the reference measurement off white paint to the unstopped full beam with the telescope at 180° and the sample removed and with the same combination of neutral density filters. The incident light (I_i) upon the samples was also referenced to the full beam at 180 $^{\circ}$ with the same conditions as above. By comparing these reference measurements, data which were taken with these references respectively could be compared by assuming that all the readings taken at one time were proportional to the readings taken at another time and differed only because of the change in sensitivity of the photomultiplier of possible change in the light source. A number of check measurements were made for the same sample at the same angles i and r only at different times and different references existing, and were found to be in good agreement when compared to these references. This procedure was necessary in order to make all measurements without removing the photomultiplier.

Moreover, improvements in the equipment and measuring technique are intended as they are indicated by the present experiments. An Eppley Thermopile and a Standard light source from the National Bureau of Standards have been received with which the light source should be calibrated. The response curve of several photomultipliers can also be calibrated in order to assure reliability and to compare results for different wavelengths. The circuits of the photomultipliers will be improved to lower noise level of about 10-11 so that a better signal to noise ratio and a little wider range is possible. The range of the 951A photomultiplier used was not great enough to measure the incident light or specular reflections without several ND filters in combinations

mentioned previously. An improved power supply for the lamp is being built and a means for holding the current through the lamp constant will be included.

The overall experimental error was not more than all digit in the second significant digit.

Another effect to be considered is the finite size of the entrance and exit apertures. The reflected intensity measured is actually an integration of the light from a cone of \$5\$ arcminutes and this collection would change with different angles of incidence. By increasing the light source and decreasing dark current, the size of openings can be decreased and the precision of the photometric measurements increased.

5. DISCUSSION OF RESULTS

5.1 Specular Front Surface Mirror

The specular reflection percentage was measured for the aluminum mirror at an angle of incidence of 20° and found to be 92% in good agreement with reference works.

- 5.2 Front Surface Mirror Smoked with 0.5mm MgO Coating
 - The MgO co ting was found to be too thin since a small specular peak occurred at i=r.
- 5.3 Front Surface Mirror Smoked with 1.0mm MgO Coating

The specular peak present in the previous sample disappeared with the increase in coating thickness. This minimum thickness of smoked MgO is therefore necessary to insure the absence of specular components in the reflection curve.

5.4 Polished Aluminum Disc Smoked with 2.0mm MgO Costing

The diffuse reflection from this sample was found to vary from Lambert's law in a certain definite pattern. At angles of incidence close to 45° the reflected light intensity was exactly proportional to the cosine of the angle of reflection within the limits of experimental error. At normal incidence, the reflected intensity decreased slightly with increasing angle of reflection as compared with the cosine, while for large angles of incidence the reflected intensities did not decrease with increasing angle of reflection as much as the cosine

of this angle. The reflected intensity distribution about the normal to a smoked MgO coated surface is therefore dependent on the angle of incidence at which the sample was illuminated.

Within the range of experimental accuracy no change could be found in the pattern of the reflection function when the incident light was filtered for different spectral regions. However, it is known that the overall intensity ratio of incident to reflected is slightly dependent on wavelength.

5.5 Polished End of Cylinder Fine Sprayed with Thin Coat of White Paint

Reflection from this sample followed the same pattern as the MgO coated sample except there was a strong reflection received at i=r and an increase in the distribution of reflected light intensity about this position.

The most interesting observation, however, was that for increasing i=r positions with respect to the normal to the surface, the reflected intensity increased becoming very large for i=r=85°. This effect was obvious visually and was compared to the specular reflection obtained from a highly polished aluminum cone of the same size, in the same position and at the same angles of incidence. The reflected intensity for this aluminum disc decreased with increasing angles of incidence as expected.

5.6 Polished End of Cylinder with Thick Heavy Coat of White Paint

Results obtained for this sample were similar to the previous white paint sample.

5.7 Polished Specular Base of Aluminum Cone.

This is the sample referred to in the comparisons made of the specular reflection from white paint and a polished aluminum cone in section 5.5 of this report.

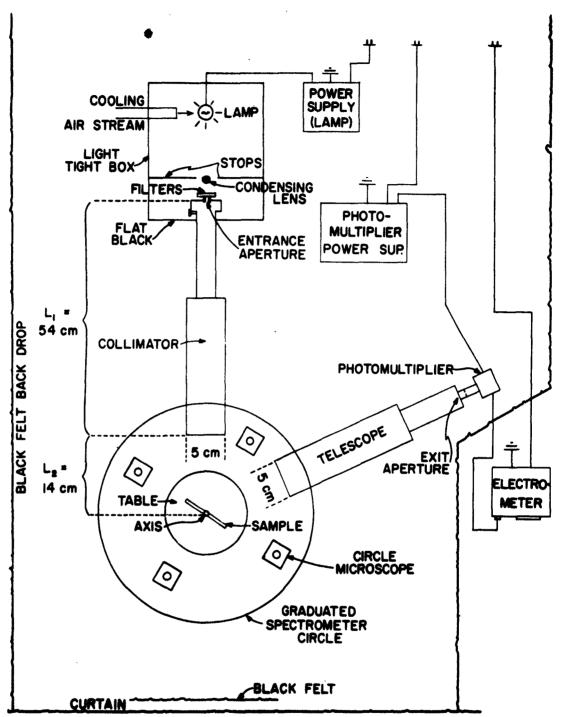
Venur Racubaushe

Dr. Werner Rambauske Principal Research Investigator Ronald Hodge
Assistant Research Physicist

APPENDIX

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Tables and Graphs



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7.7 1.4 1.7

Figure 1. Schematic Diagram of Photometric Equipment.

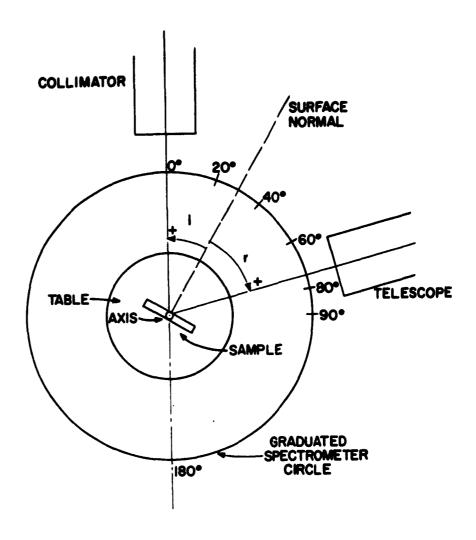
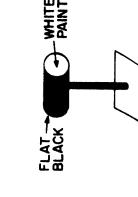
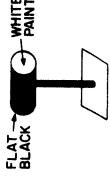


Figure 2. Schematic Diagram Showing Orientation of Sample and Defining Angles of Incidence and Reflection.

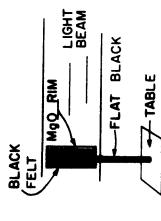


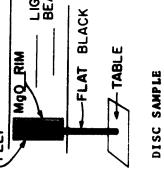


CYLINDER SAMPLE

CONE SAMPLE

-





FLAT BLACK



Figure 3. Schematic Diagrams of Samples.

IMPROVED DISC SAMPLE

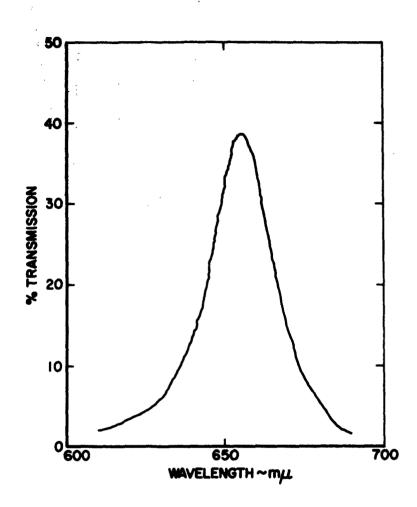


Figure 4. Transmission of Optics Technology Filter #656

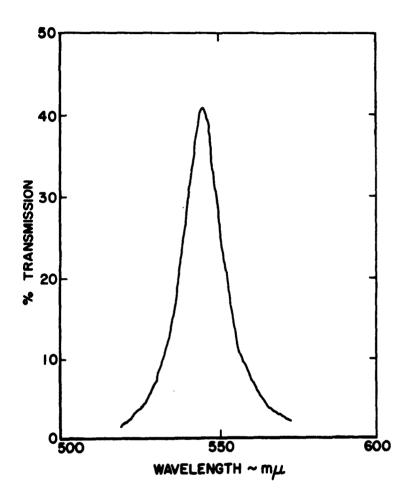


Figure 5. Transmission of Optics Technology Filter #546

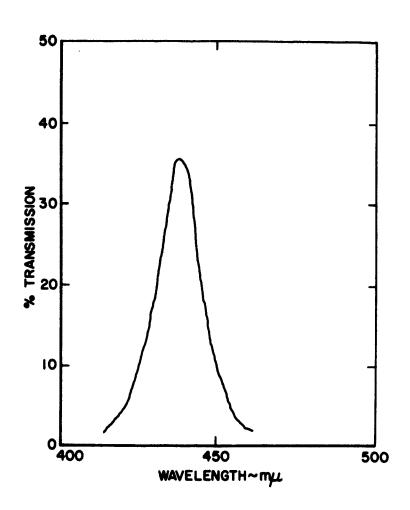


Figure 6. Transmission of Optics Technology Filter #436



Figure 7. Gaertner L124 High Precision Spectrometer and Apparatus.



Figure 8. Spectrometer with Sample on Table.

TABLE 1. RATIOS Ir1/Ir2

.

Sample: MgO #3, No Filter

r1: r2	i=0•	i=20°	i=40°	i=60°	i=80°	COST	$f(r) = [1-1.3 \sin^2(\frac{r}{2})]\cos r$
0.:10.			1.03	1.02	1.01	1.02	1.03
10.:20			1.07	1.03	1.02	1.05	1.08
20.:30.		1.11	1.07	1.07	1.02	1.09	1.14
30 : 40		1.15	1.12	1.09	1.03	1.13	1,22
40.:50	1.20	1.22	1.20	1.13	1.02	1.19	1,32
.09:.05	1.32	1.32	1.30	1.17	1.01	1.29	1.46
.00:09	1.55	1.54	1.47	1.28	1.05	1.46	1.72
70.:80	2.00	2.01	1.90	1.65		1.97	2.43

TABLE 2. RATIOS I_{r_1}/I_{r_2} (i=0°)

	MgO #3	E# OoM	₩ 0°₩	MgO #3	3 A	
r1: r2	No Filter	Blue #436	Green #546	Red #656	No Filter	Cos r
0.:10						1.02
10 .: 20						1.05
20.:30						1.09
30.:40.						1.13
40.:50	1.20	1.23	1.19	1.23	1.22	1.19
£00:00	1.32	1.39	1.35	1.36	1.30	1.29
.04:09	1.55	1.55	1.65	1.64	1.58	1.46
700:80	2.00	2.56	2.22		2.55	1.97

TABLE 3. RATIOS Ir1/Ir2

(i=20°)

r1: r2	MgO#3 No Filter	MgO #3 Blue #436	MgO #3 Green #546	MgO #3 Red #656	Cos r
0.:10					1.02
10.:20.					1.05
20.:30	1.11	1.10	1.11	1.14	1.09
30.:40.	1.15	1.14	1.14	1.20	1.13
40.:50	1.22	1.23	1.20	1.21	1.19
•09:•05	1.32	1.35	1.32	1.41	1.29
.02:.09	1.54	1.56	1.56	1.57	1.46
70.:80	2.01	2.37	2.17	2.53	1.97

TABLE 4. RATIOS Ir1/1r2

			(i=40°)			
r1: r2	MgO #3 No Filter	ligo #3 Blue #436	MrG #3 Green #546	NgO #3	(at i=45°) W.P. #1 No Filter	Cos r
0.:10	1.03	1.02	1.04	1.02	1.03	1.02
10.:20	1.07	1.05	1.06	1.06	. 1.05	1.05
20.:30.	1.07	1.06	1.07	1.10	1.07	1.09
30 :40	1.12	1.16	1,12	1.13	Spec.	1.13
40°:50°	1.20	1.16	1.21	1.17	Spec.	1.19
.09:.05	1.30	1.30	1.32	1.37	Spec.	1.29
.04:.09	1.47	1.50	1.45	1.45	1.63	1.46
70°:80°	1.90	2.72(?)	2.05	2.26	2.51	1.97

TABLE S. RATIOS Ir1/1r2

(i=60°)

0*:10* 1.02 1.00 1.01 1.01 10*:20* 1.03 1.04 1.05 1.03 1.03 20*:30* 1.07 1.01 1.06 1.12 1.05 30*:40* 1.09 1.10 1.08 1.10 1.09 40*:50* 1.13 1.17 1.11 Spec. 50*:60* 1.17 1.12 1.11 Spec. 60*:70* 1.28 1.36 1.35 1.58 Spec. 70*:80* 1.65 2.23 1.70 2.50 Spec.	r1: r2	NgO #3 No Filter	NgO #3 Blue #436	NgO #3 Green #546	NgO #3 Red #656	(i=85°) %.P. #1 No Filter	Cos r
1.03 1.04 1.05 1.05 1.07 1.01 1.06 1.12 1.09 1.10 1.08 1.10 1.13 1.17 1.11 1.11 1.17 1.19 1.20 1.24 1.28 1.36 1.35 1.58 1.65 2.23 1.70 2.50	0.10	1.02	1.02	1.00	1.00	1.01	1.02
1.07 1.01 1.06 1.12 1.09 1.10 1.08 1.10 1.13 1.17 1.11 1.11 1.17 1.19 1.24 1.24 1.28 1.36 1.35 1.58 1.65 2.23 1.70 2.50	10*:20*	1.03	1.04	1.05	1.05	1.03	1.05
1.09 1.10 1.08 1.10 1.13 1.17 1.12 1.11 1.17 1.19 1.20 1.24 1.28 1.36 1.35 1.58 1.65 2.23 1.70 2.50	20.:30.	1.07	1.01	1.06	1.12	1.05	1.09
1.13 1.17 1.12 1.11 1.17 1.19 1.20 1.24 1.28 1.36 1.35 1.58 1.65 2.23 1.70 2.50	30 : 40	1.09	1.10	1.08	1.10	1.09	1,13
1.17 1.19 1.24 1.28 1.36 1.35 1.58 1.65 2.23 1.70 2.50	40.:50	1.13	1.17	1.12	1.11	Spec.	1.19
1.28 1.36 1.58 1.65 2.23 1.70 2.50	.09:.05	1.17	1.19	1.20	1.24	Spec.	1.29
1.65 2.23 1.70 2.50	60.:70	1.28	1.36	1.35	1.58	Spec.	1.46
	70.:80	1.65	2.23	1.70	2.50	Spec.	1.97

TABLE 6. BACKGROUND OFF SAMPLE SUPPORT

Telescope Setting (=i+r)	Background Current Off Shaft	Dark Current
35 °	2.22 x 10 ⁻⁹ amps	1.90 x 10 ⁻⁹ amps
4 0 °	$2.20 \times 10^{-9} \text{ amps}$	1.90 x 10 ⁻⁹ amps
45°	$2.18 \times 10^{-9} \text{ amps}$	1.90 x 10 ⁻⁹ amps
50°	2.18 x 10 ⁻⁹ amps	1.90 x 10 ⁻⁹ amps
60°	$2.18 \times 10^{-9} \text{ amps}$	1.90 x 10 ⁻⁹ amps
70°	$2.16 \times 10^{-9} \text{ amps}$	1.90 x 10 ⁻⁹ amps
80 °	$2.15 \times 10^{-9} \text{ amps}$	1.90 x 10 ⁻⁹ amps
90°	$2.13 \times 10^{-9} \text{ amps}$	$1.90 \times 10^{-9} \text{ amps}$
100°	$2.13 \times 10^{-9} \text{ amps}$	1.90×10^{-9} amps
110°	$2.12 \times 10^{-9} \text{ amps}$	1.90 x 10 ⁻⁹ amps
120°	$2.12 \times 10^{-9} \text{ amps}$	1.90 x 10 ⁻⁹ amps
130°	$2.22 \times 10^{-9} \text{ amps}$	1.90 x 10 ⁻⁹ amps
140°	2.32 (?)	1.90 x 10 ⁻⁹ amps
150°	2.42 (?)	1.90 x 10 ⁻⁹ amps
160°	(?)	1.90×10^{-9} amps

SPECTROMETER DATA

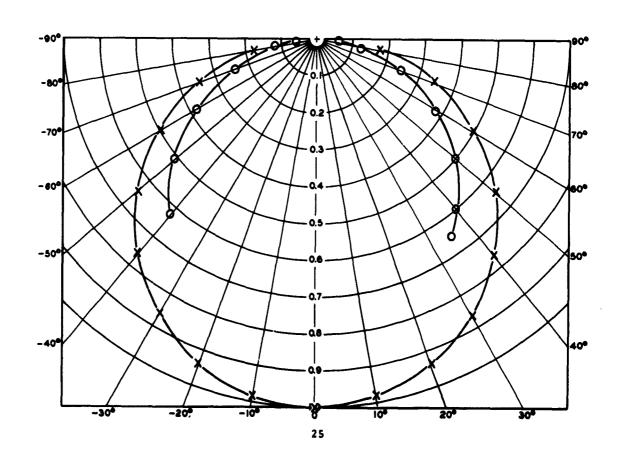
Contract AF 33(657)-9014

	number oflection s:	l Diffuse	Incidence Filter Sample Dimensions Coating	N D	=0° one iffuse Standard isc. 2r =2.5cm g0 #3, t=2mm
Adj. R	nt Light ef. for I _i j. for ref.)	$\frac{\text{Ii} = 0.298 \cos 0^{\circ}}{1.66 \times 10^{-7}}$ $\frac{0.242}{}$	Reference: For reflected Filter b.c. Lamp I'r adj.	$\begin{array}{c} \text{light } \overline{1} \\ \overline{N} \\ \overline{1} \\ \overline{5} \end{array}$	t i=0°, r=45° r=1.41 x 10-7 one .34 x 10-9 .00 volts .35 x 10-7
rI	_r x10 ⁷ (amps)	Lamp Voltage(volts) b.c.x109(amps)	I'rx107(amps) (I' _r /I' ₁)x10 ⁷
35° 40° 50° 60° 70° 80° 85° -40° -50° -60° -70° -80° -85°	1.63 1.51 1.26 0.960 0.625 0.312 0.169 1.57 1.28 0.960 0.610 0.300 0.166	5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00	1.31 1.32 1.34 1.34 1.33 1.33 1.33 1.35 1.37 1.37	1.57 1.45 1.21 0.920 0.592 0.296 0.153 1.51 1.23 0.920 0.581 0.284 0.150	6.49 5.99 5.00 3.80 2.45 1.22 0.632 6.24 5.08 3.80 2.40 1.17 0.619

Function of the Angle of Reflection $f(r)=(I'_r/I'_i) \times 10^7$

Record Number 1

O f(r) Measured X - X f(r) = cos r



SPECTROMETER DATA

Contract AF 33(657)-9014

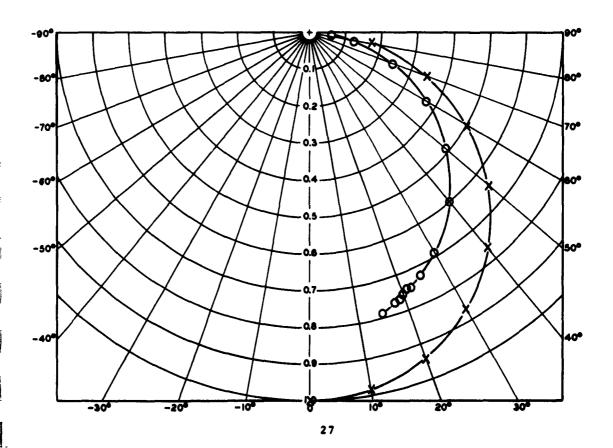
	Reflection	<u>Diffuse</u>	Incidence Filter Sample Dimensions Coating	Disc.	se Standard 2r=2,5cm 3, t=2mm
Adj.	dent Light Ref. for I _i adj. for ref.)	I;=0.298 cos 20° 1.66 x 10-7 0.228	Reference: For reflected Filter b.c. Lamp I'r adj.	light $\frac{I_r = 1}{None}$ $\frac{1.34}{5.00}$	x 10-9 volts x 10-7
r	$I_x x 10^7 (amps)$	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107(amps	$(I_T'/I_j') \times 10^7$
15° 20° 25° 30° 40° 50°	1.87 1.80 1.72 1.63 1.42 1.17	5.00 5.00 5.00 5.00 5.00 5.00	1.35 1.36 1.37 1.37 1.37	1.80 1.74 1.66 1.57 1.37	7.89 7.63 7.28 6.89 6.01 4.91
60° 70° 80° 85° 86° 87°	0.890 0.580 0.297 0.168 0.141 0.118 0.097	5.00 5.00 5.00 5.00 5.00 5.00 5.00	1.37 1.37 1.37 1.37 1.37 1.37	0.849 0.551 0.274 0.148 0.121 0.099 0.079	3.72 2.42 1.20 0.649 0.530 0.434
90° 18° 19° 20° 21° 22°	0.057 1.82 1.81 1.79 1.78 1,77	5.00 5.00 5.00 5.00 5.00 5.00	1.37 1.37 1.37 1.37 1.37	0.040 1.76 1.75 1.73 1.72	0.175 7.72 7.67 7.59 7.54 7.50

Function of the Angle of Reflection $f(r)=(I'_r/I'_i) \times 10^7$

Record Number 2

O f(r) Measured

X f(r) = cos r

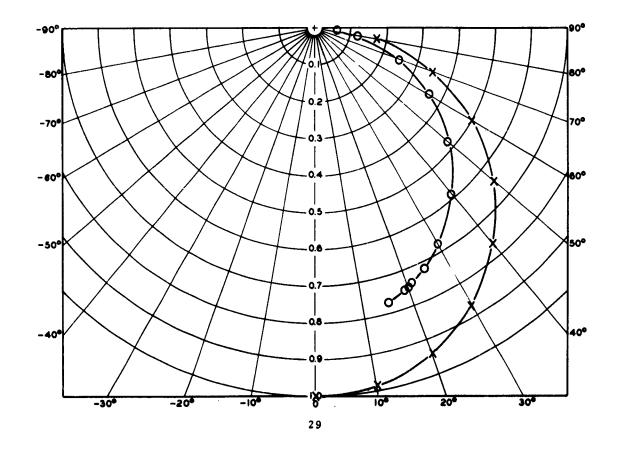


Record number 3 Type Reflection Diffuse Remarks:		Incidence Filter Sample Dimensions Coating		i=20° N.D. #0.5 Diffuse Standard Disc, 2r=2.5cm MgO #3, t=2mm	
Adj.	ent Light Ref. for I _i dj. for ref.)	<u>li=0.0943 cos 20°</u> 1.66 x 10-7 0.0721	Reference: For reflected Filter b.c. Lamp I'r adj.	light	at i=0°, r=45° I _r =1.41 x 10-7 None 1.34 x 10-9 5.00 volts 1.35 x 10-7
ŗ	I _x x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx10	$I(amps) (I'_T/I'_i) \times 10^7$
15° 19° 20° 21° 25° 30° 40° 50° 60° 70° 85°	0.575 0.560 0.559 0.554 0.533 0.507 0.442 0.365 0.278 0.191 0.102 0.061	5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00	1.41 1.41 1.41 1.41 1.41 1.41 1.41 1.41	0.554 0.542 0.542 0.532 0.516 0.492 0.348 0.261 0.175 0.045	3 7.53 2 7.51 7 7.44 6 7.15 9 6.79 5 5.89 8 4.82 1 3.62 2 43 1 19

Record Number 3

O f(r) Measured

X f(r) = $\cos r$

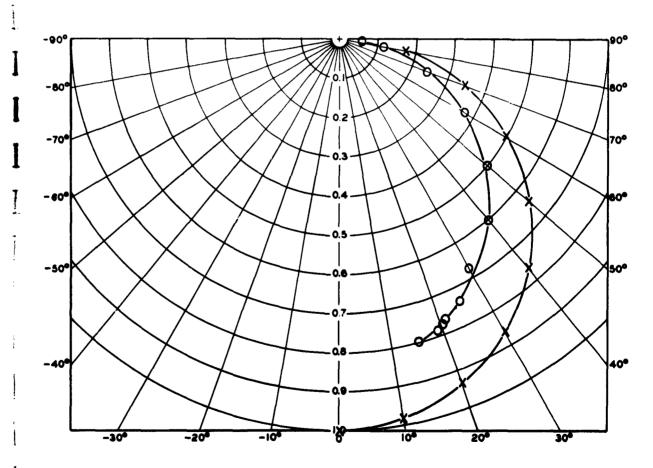


Record number Type Reflection Remarks:		Diffuse	Incidence Filter Sample Dimensions Coating		i=20° N.D. #1 Diffuse Standard Disc, 2r=2.5cm Mg0 #3, t=2mm	
Adj. R	nt Light ef. for Ii j. for ref.)	1:=0.0288 cos 20° 1.66 x 10-7 0.0236	Reference: For reflected Filter b.c. Lamp I'r adj.	light	at i=0°, r=45° I _r =1.48 x 10-7 None 1.50 x 10-9 5.00 volts 1.45 x 10-7	
rI	rx10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'r×107	$(amps) (I'_T/I'_i) \times 10^{7}$	
15° 19° 20° 21° 25° 30° 40° 50° 60° 70° 80° 85° 87°	0.207 0.200 0.197 0.195 0.188 0.177 0.161 0.135 0.105 0.074 0.044	5.00 4.98 4.98 4.98 4.98 5.00 5.01 5.00 5.00 5.00 5.00 4.99	1.41 1.43 1.43 1.43 1.43 1.43 1.43 1.43	0.190 0.187 0.184 0.175 0.160 0.143 0.018 0.088 0.027 0.014	7 7.92 7 7.80 7 7.71 6 7.42 0 6.78 6 06 8 5.00 8 3.73 7 2.42 7 1.14 16 0.619	

Record Number 4

O O f(r) Measured

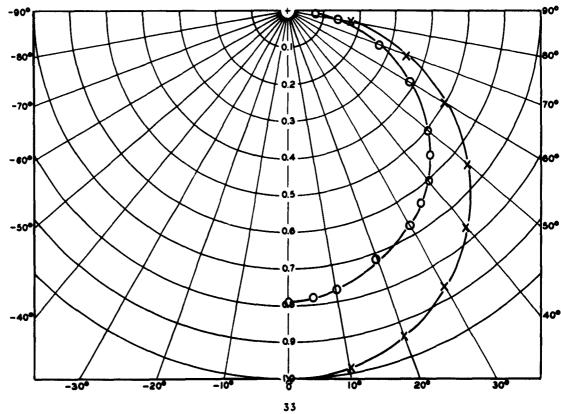
X $f(r) = \cos r$



Type Remark Incide	number eflection s: nt Light ef. for Ii	5 Diffuse I:=0.298 cos 40° 1.66 x 10°7 0.199	Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	light	i=40° None Diffuse Standard Disc. 2r=2.5cm MgO #3. t=2mm at i=0°. r=45° I _{r=1.48} x 10-7 None 1.50 x 10-9 5.00 volts 1.45 x 10-7
r	rx10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx10	$^{7}(amps) \left(I'_{T}/I'_{i}\right) \times 10^{7}$
-5° 0° 5° 10° 20° 35° 40° 45° 60° 70° 85°	1.61 1.60 1.58 1.55 1.45 1.36 1.28 1.21 1.11 1.01 0.808 0.557 0.300 0.174	4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.98	1.53 1.53 1.53 1.53 1.53 1.56 1.56 1.56 1.53 1.53	1.59 1.58 1.56 1.53 1.43 1.27 1.20 1.10 1.00 0.52 0.27 0.15	7.94 7.84 7.69 7.19 6.73 6.38 6.03 5.53 5.03 0.387 5.404 6.1.39

Record Number 5

O f(r) Measured X f(r) = cos r

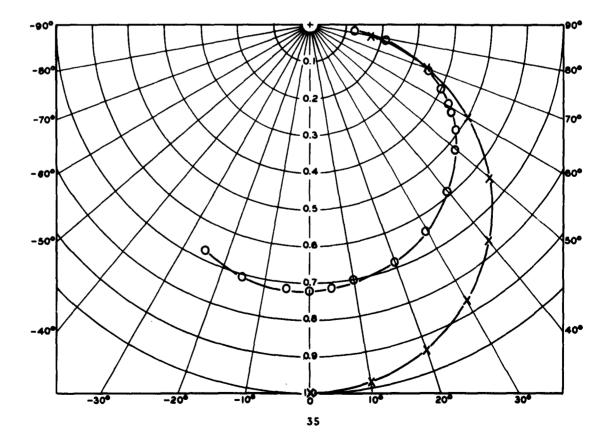


Type Rema read Incid Adj.	Reflection (Ketlection (Ketlec	1 it face change in ref. du	Coating	light Ir No	
r	I _T x10 ⁷ (amps)	Lamp Voltage(vo	lts) b.c.x109(amps)	I'_x107(a	$nps) \left(\mathbf{I_T'} / \mathbf{I_J'} \mathbf{x} \mathbf{10^7} \right)$
~25°	0.790	4.98	1.90	0.784	6.78
-15°	0.824	4.98	1.90	0.818	7.08
-5°	0.840	4.98	1.90	0.834	7,21
0 °	0.840	4.98	1.90	0.834	7,21
5 °	0.835	4.98	1.90	0.829	7.17
10°	0.821	4.98	1.90	0.815	7.05
20	0.798	4.98	1.90	0.793	6.86
30°	0.748	4.98	1.90	0.742	6,42
40°	0.690	4.98	1.90	0.683	5.91
50°	0.615	4.98	1.91	0.607	5,25
55°	0.578	4.98	1.91	0.569	4,92
59°	0.535	4.98	1.91	0.525	4.54
60°	0.527	4.98	1.91	0.517	4.47
61°	0.518	4.98	1.91	0.508	4.39
65°	0.475	4.98	1.91	0.463	4.00
70°	0.418	4.98	1.91	0.405	3.50
80°	0.262	4.98	1.91	0.245	2.12
85	0.161	4.98	1.91	0.141	1.22
87°	0.119	4.98	1.91	0.098	0.85
89°	0.078	4.97	1.91	0.057	0.49
90°	0.059	4.97	1.91	0.037	0.32

Record Number 6

O f(r) Measured

X f(r) = $\cos r$

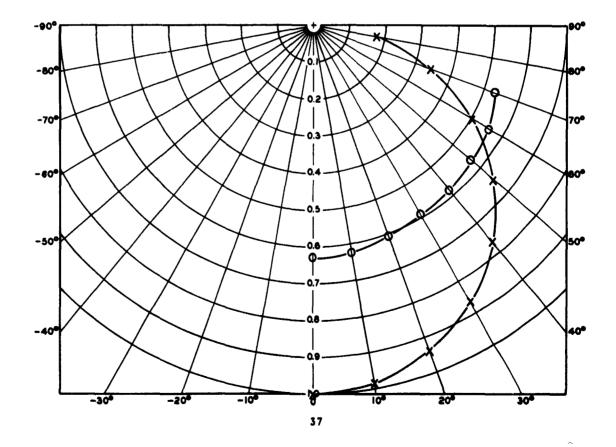


Record number 7 Type Reflection Diffuse Remarks: Sample not perfectly plane		Incidence Filter Sample Dimensions Coating	Dis		
Adj. I	ent Light Ref. for Ii dj. for ref.)	1.66 x 10-7 0.0484	Reference: For reflected Filter b.c. Lamp I'r adj.	1ight Ir= Non 2.3 5.0	
r	I _r x10 ⁷ (amps)	Lamp Voltage(volts) b.c.x109(amps)	I'rx107(am)	ps) (I' _T /I' ₁)x10 ⁷
-45° -40° -30° -20° -10°	0.296 0.310 0.323 0.331 0.335 0.330 0.327	5.00 5.01 5.00 5.00 5.00 5.00 5.00	2.33 2.33 2.33 2.33 2.34 2.34 2.34	0.304 0.301	6.28 6.22
20° 30° 40° 50° 60°	0.327 0.321 0.315 0.307 0.301 0.298	5.00 5.00 5.00 5.00 5.00 5.00	2.34 2.34 2.33 2.33 2.33 2.33	0.295 0.289 0.281 0.275 0.271	6.10 5.97 5.81 5.68 5.60 5.33

Record Number 7

O----O f(r) Measured

X----X f(r) = cos r

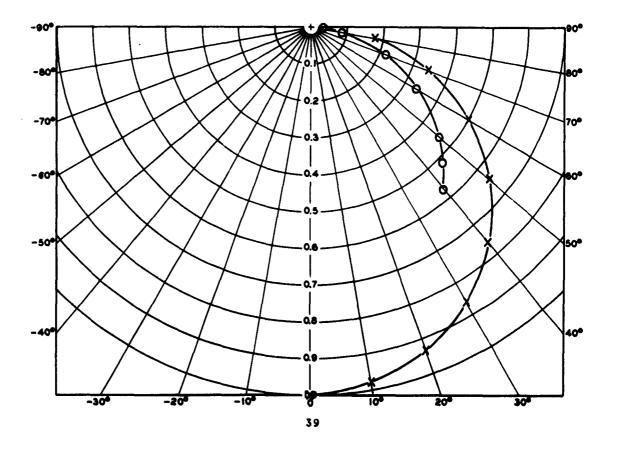


Type Remar 1.76 Incid Adj.	d number Reflection ks: Ref. for x 10-7 ent Light Ref. for Ii dj. for ref.	8 Diffuse Ir without filter Ii=0.00640 1.66 x 10-7 0.00679	Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	Diffi Disc MgO light I_=0 0.T. 2.28 5.00	#436 blue use Standard 2r=2.5cm #3. t=2mm =0°. r=45° .0593 x 10-7 #436 blue x 10-9 volts 78 x 10-7
r	I _x x10 ⁷ (amps)	Lamp Voltage (volts) b.c.x109(amps)	I'rx107(amp	i) (I' _r /I' _j)x10 ⁷
40° 45° 50° 60° 70° 80° 85° 40°	0.0633 0.0593 0.0559 0.0473 0.0388 0.0302 0.0264 0.0630	4.99 4.99 4.99 4.98 4.98 4.98 4.98	2.28 2.28 2.26 2.28 2.28 2.26 2.26 2.26	0.0390 0.0351 0.0316 0.0227 0.0146 0.0057 0.0018 0.0017	5.75 5.17 4.65 3.34 2.15 0.84 0.27 0.25
-50° -60° -70° -80°	* 0.0650 * 0.0570 * 0.0492 * 0.0412 * 0.0319	4.98 4.98 4.98 4.98 4.98	2.43 2.43 2.43 2.43 2.43 2.43		

Record Number 8

O----O f(r) Measured

X-----X f(r) = cos r

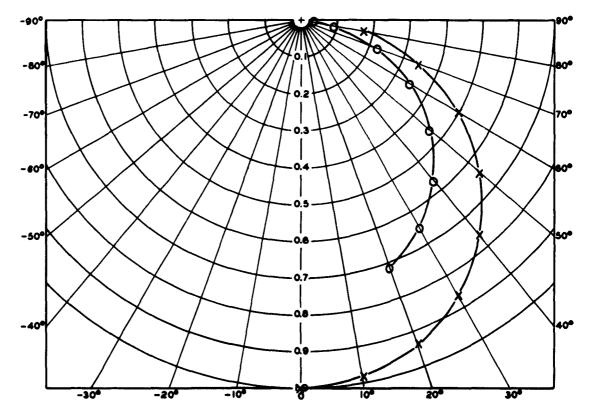


Type Reflection Diffuse Remarks: Changed setting before second 20° reading Incident Light 0.00602 Adj. Ref. for Ii 1.66 x 10-7 I'i (adj. for ref.) 0.00643		Incidence Filter Sample d Dimensions Coating Reference: For reflected light Filter b.c. Lamp I'r adj.		i=20° O.T. #436 blue Diffuse Standard Disc. 2r=2.5cm MgO #3. t=2mm at i=0°. r=45° Ir=0.0607 x 10-7 O.T. #436 blue 2.33 x 10-9 5.00 volts O.0381 x 10-7		
						7
20° 30°	0.0700 0.0660	4.98	2.33	0.04	20	7.17 6.53
40° 50° 60°	0.0608 0.0540 0.0467	4.98 4.98 4.98	2.33 2.35 2.35	0.03 0.02 0.02	98 21	5.71 4.63 3.44
70° 80° 85° 20°	0.0388 0.0312 0.0278 0.0710	4.98 4.98 4.99 5.00	2.35 2.37 2.37 2.40	0.01 0.00 0.00	60	2.21 0.93 0.36

Record Number 9

O-O f(r) Measured

X-X f(r) = cos r

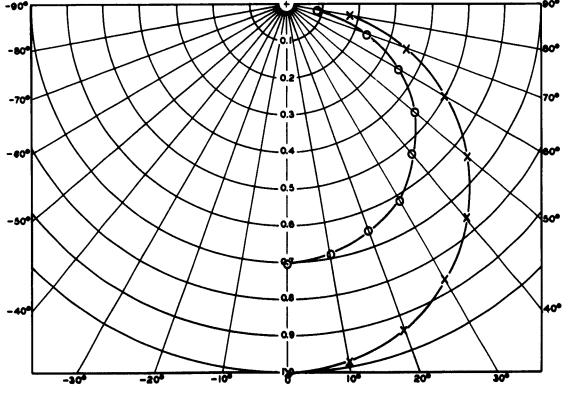


Type Reflection Diffuse Remarks:			Incidence Filter Sample Dimensions Coating Reference: For reflected ligh Filter b.c. Lamp I'r adj.		i=40° O.T. #436 blue Diffuse Standard Disc. 2r=2.5cm MgO #3, t=2mm at i=0°, r=45° I _r =0.0607 x 10-7 O.T. #436 blue 2.40 x 10-9 4.98 volts 0.0386 x 10-7	
		1.66 x 10-7				
Ī	Irx107(amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107(a	mps) (I' _r /I' _j)x10 ⁷	
0° 10° 20° 30° 40° 50° 60° 70° 80°	0.0640 0.0632 0.0607 0.0585 0.0540 0.0500 0.0446 0.0385 0.0308	5.00 4.99 4.99 4.99 4.99 4.99 4.99 4.99	2.43 2.43 2.44 2.44 2.45 2.45 2.44 2.44	0.0373 0.0367 0.0348 0.0328 0.0282 0.0243 0.0187 0.0125 0.0046	7.04 6.92 6.57 6.19 5.32 4.58 3.53 2.36 0.87	

Record Number 10

O f(r) Measured

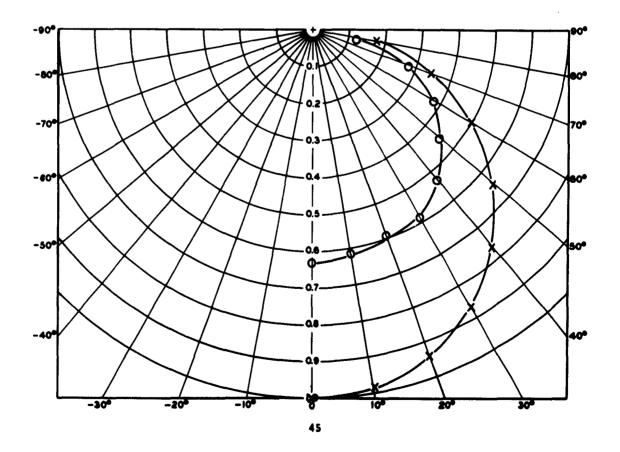
X f(r) = cos r



Record number Type Reflection Remarks:			Incidence Filter Sample Dimensions Coating		i=60° O.T. #436 blue Diffuse Standard Disc. 2r=2.5cm MgO #3, t=2mm	
Adj. R	ent Light Ref. for I _i lj. for ref.)	Ii=0.00320 1.66 x 10-7 0.00344	Reference: For reflected Filter b.c. Lamp I'r adj.	light	0.T. 4 2.43 x 4.98 y	607 x 10-7 436 blue 10-9
r I	x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'r×10	⁷ (amps)	(I' _r /I' _i)x10 ⁷
-20° -10° 0° 10° 20° 30° 40° 50° 60° 70° 80° -20°	0.0470 0.0478 0.0476 0.0470 0.0461 0.0456 0.0437 0.0412 0.0387 0.0358 0.0312	4.98 4.99 4.99 4.99 4.99 4.99 4.99 4.99	2.43 2.42 2.41 2.40 2.40 2.40 2.40 2.40 2.41 2.41	0.02 0.02 0.02 0.01 0.01 0.01	12 04 01 82 56 31	6.28 6.16 5.93 5.84 5.29 4.53 3.81 2.79 1.25

Record Number 11

O f(r) Measured X - X $f(r) = \cos r$

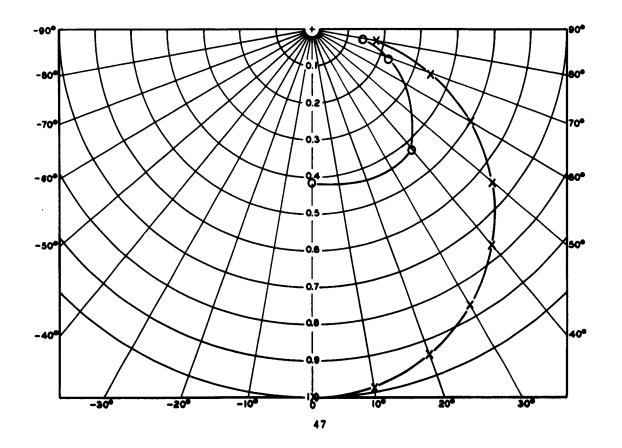


Type Reflection		Incidence Filter Sample Dimensions Coating	•	i=80° O.T. #436 blue Diffuse Standard Disc, 2r=2.5cm Mgo #3, t=2mm	
		Reference: For reflected light Filter b.c. Lamp I'r adj.		at i=0° r=45° I _r =0.0607 x 10-7 0.T. #436 blue 2.43 x 10-9 4.98 volts 0.0383 x 10-7	
r	I _r x10 ⁷ (amps)	Lamp Voltage(volts	b.c.x109(amps)	I' _r x107	(amps) (I' _T /I' ₁)x10 ⁷
-40° 0° 40° 70° 80°	0.0304 0.0308 0.0306 0.0303 0.0295	4.98 4.98 4.98 4.98 4.98	2.41 2.40 2.40 2.40 2.40	0.005 0.005 0.002 0.001	1 4.25 7 2.25

Record Number 12

O----O f(r) Measured

X----X f(r) = cos r

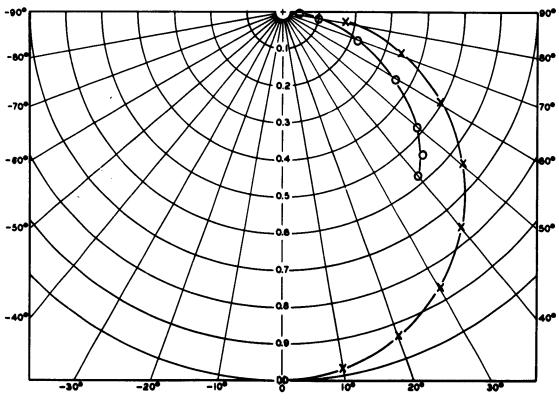


Record number 13 Type Reflection Diffuse Remarks: Ref. for I without filter 1.73 x 10-7		Incidence Filter Sample Dimensions Coating	i=0° O.T #546 green Diffuse Standard Disc. 2r=2.5cm MgO #3. t=2mm		
Adj.	ent Light Ref. for Ii dj. for ref.	$ \begin{array}{c} 1_1 = 0.0138 \\ 1.66 \times 10^{-7} \\ 0.0144 \end{array} $	Reference: For reflected Filter b.c. Lamp I'r adj.	l light $\frac{I_{r}=0}{0.T}$, $\frac{2.33}{5.00}$	-0° r-45° .104 x 10-7 #546 green x 10-9 volts 0 x 10-7
r	I _r x10 ⁷ (amps)	Lamp Voltage(vol	ts) b.c.x109(amps)	I'rx107(amp	s) (I' _r /I' _i)x10 ⁷
45° 40° 50° 60° 70° 85° 40° -40° -50° -70° -80° -80°	0.104 0.109 0.0933 0.0758 0.0562 0.0390 0.0312 0.109 0.109 0.0923 0.0729 0.0548 0.0380 0.0302	5.00 5.00 5.00 5.01 5.01 5.01 5.00 5.01 5.02 5.00 5.00 5.00 5.00	2.24 2.24 2.24 2.24 2.24 2.24 2.24 2.23 2.23	0.078 0.083 0.0696 0.0517 0.0313 0.0141 0.0063	5.42 5.76 4.83 3.59 2.17 0.98 0.44 5.76

Record Number 13

O-O f(r) Measured

 $X \longrightarrow X$ $f(r) = \cos r$

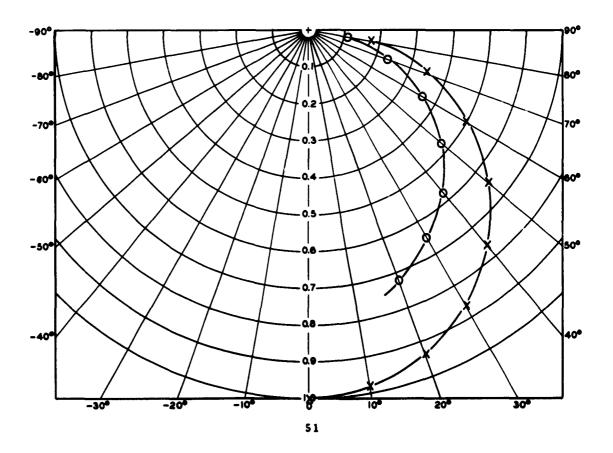


Type Reflection		Incidence Filter Sample Dimensions Coating	<u>.</u>	i=20° 0.T. #546 green Diffuse Standard Disc. 2r=2.5cm MgO #3, t=2mm	
		Reference: For reflected Filter b.c. Lamp I'r adj.	light	ight $ \frac{\text{at i=0}^{\circ}, \text{ r=45}^{\circ}}{\text{I}_{\text{r}=0,104} \times 10^{-7}} $ $ 0.7. $	
r	Irx107(amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107((smps) (I' _T /I' _j)x10 ⁷
20° 30° 40° 50° 60° 70° 80° 20°	0.126 0.116 0.104 0.091 0.074 0.0552 0.0386 0.125	5.00 5.00 4.99 4.99 4.99 4.98 4.98	2.26 2.26 2.26 2.26 2.26 2.26 2.26	0.100 0.090 0.079 0.066 0.050 0.032	1 2.33

Record Number 14

O---O f(r) Measured

 $X \longrightarrow X$ $f(r) = \cos r$



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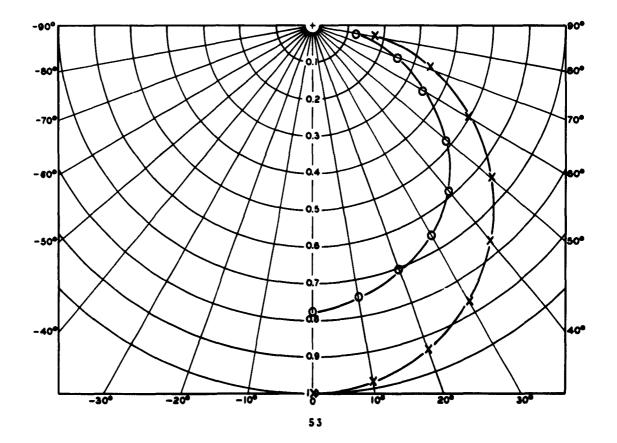
Type Remai	Reflection rks: dent Light Ref. for Ii adj. for ref.	15 Diffuse I _i =0.0106 1.66 x 10 ⁻⁷ 0.0111	Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	Diffu Disc. MgO # 1ight I = 0. 0.T. 2.20 4.98	#546 green se Standard 2r=2.5cm 3. t=2mm 0°. r=45° 102 x 10-7 #546 green x 10-9 volts x 10-7
r	I _r x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'_x107(amps)	$(I_T'/I_i)x10^7$
0°10°20°30°40°50°60°70°80°0°	0.111 0.108 0.103 0.097 0.088 0.0767 0.0659 0.0521 0.0379 0.111	5.00 5.00 5.00 4.99 4.98 4.99 5.02 5.00 5.00	2.21 2.21 2.21 2.21 2.21 2.22 2.23 2.24 2.25	0.086 0.083 0.078 0.073 0.065 0.0539 0.0408 0.0281	7.75 7.48 7.03 6.58 5.86 4.86 3.68 2.53 1.23

the contract was a second

Record Number 15

O----O f(r) Measured

X-----X f(r) = cos r



Contract AF 33(657)-9014

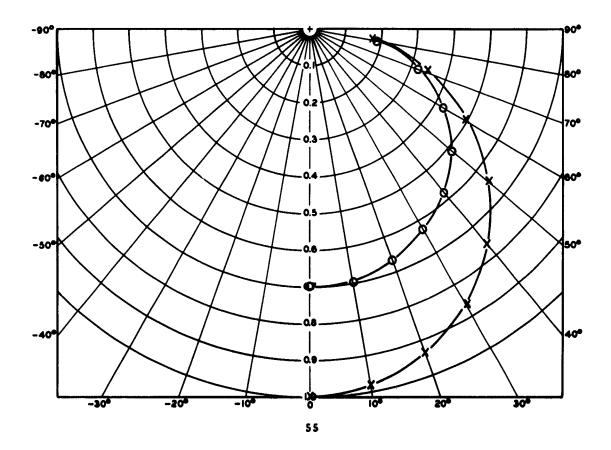
	d number Reflection ks:	16 Diffuse	Incidence Filter Sample Dimensions Coating	Diffu Disc	#546 green use Standard 2r=2.5cm 3, t=2mm
Adj.	ent Light Ref. for I _i dj. for ref.]	<u>Ii = 0.00689</u> <u>1.66 x 10-7</u> 0.00709	Reference: For reflected Filter b.c. Lamp I'r adj.	1ight <u>I=0</u> 0.T. 2.32 5.00	**************************************
T	I _r x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107(amps) (I' _r /I' _i)x10 ⁷
-20° -10° 0° 10° 20° 30° 40° 50° 60° 70° 80° -20°	0.0725 0.0738 0.0738 0.0735 0.0710 0.0681 0.0642 0.0598 0.0538 0.0466 0.0377	5.00 5.00 5.00 5.00 5.00 5.00 4.99 4.99 4.99	2.25 2.25 2.25 2.25 2.25 2.25 2.25 2.25	0.0496 0.0495 0.0471 0.0443 0.0410 0.0365 0.0303 0.0224 0.0132	6.99 6.98 6.64 6.25 5.78 5.15 4.27 3.16 1.86

-1

Record Number 16

O—O f(r) Measured

 $X \longrightarrow X$ $f(r) = \cos r$

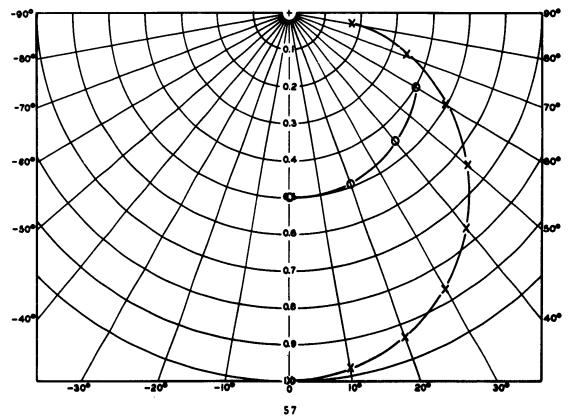


Type Reflection		Incidence Filter Sample Dimensions Coating	O.T. Difi	i=80° 0.T. #546 green Diffuse Standard Disc. 2r=2.5cm MgO #3, t=2mm at i=0°. r=45° I==0.105 x 10-7 0.T. #546 green 2.28 x 10-9 5.00 volts 0.082 x 10-7	
		Reference: For reflected Filter b.c. Lamp I'r adj.	1ight 1 = 0.T. 2.21 5.01		
Ţ	I _T x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107(amp	os) (I' _T /I' ₁)x10 ⁷
-40° -20° 0° 20° 40° 60°	0.0374 0.0382 0.0382 0.0379 0.0368 0.0365	5.00 5.00 5.00 5.00 5.00 5.00	2.28 2.29 2.32 2.32 2.32 2.32	0.0128 0.0127 0.0117 0.0104	4.99 4.95 4.56 4.06

Record Number 17

O f(r) Measured

X----X f(r) = cos r



Contract AF 33(657)-9014

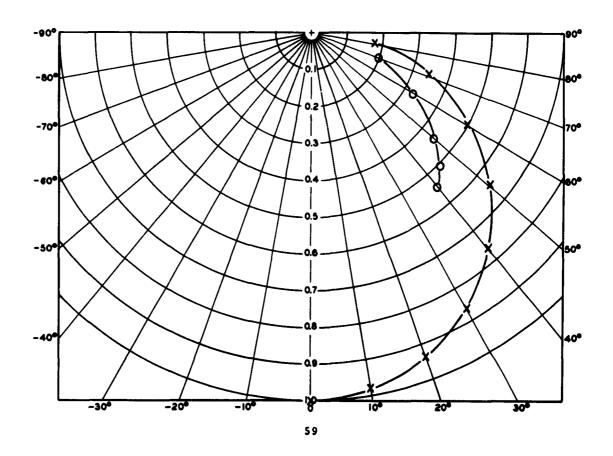
Record number			Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	i=0° O.T. #656 red Diffuse Stands Disc. 2r=2.5cm MgO #3, t=2mm at i=0°, r=45° I_=0.0485 x 10 O.T. #656 red 2.31 x 10-9 4.98 volts O.0270 x 10-7	
r	$I_{r} \times 10^{7} (amps)$	Lamp Voltage(volts)	b.c.x109(amps)	I'r×107(a	mps) (I'r/I'j)x107
40° 45° 50° 60° 70° 40°	0.0520 0.0485 0.0461 0.0406 0.0345 0.0518	5.00 4.97 4.98 4.98 4.98 4.98	2.32 2.32 2.32 2.32 2.32 2.32	0.0263 0.0245 0.0214 0.0157 0.0096	5.42 5.05 4.41 3.24 1.98

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Record Number 18

O f(r) Measured

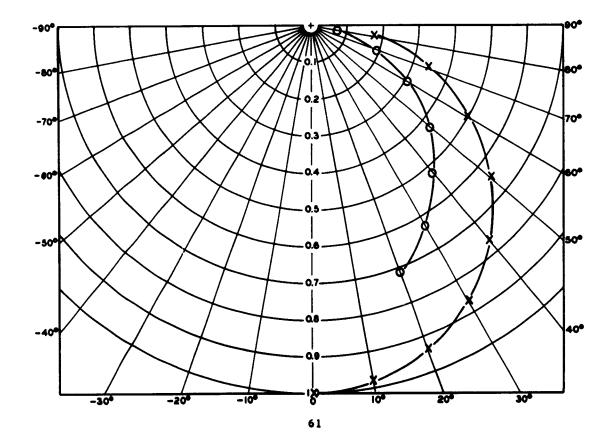
 $X \longrightarrow X$ $f(r) = \cos r$



Record number 19 Type Reflection Diffuse Remarks: Incident Light $I_{i=0.00432}$ Adj. Ref. for I_{i} 1.66 x 10-7 0.00442			Incidence Filter Sample Dimensions Coating		i=20° O.T. #656 red Diffuse Standard Disc. 2r=2.5cm MgO #3. t=2mm	
		Reference: For reflected light Filter b.c. Lamp I'r adj.		at i=0° r=45° Ir=0.0502 x 10-7 O.T. #656 red 2.45 x 10-9 5.00 volts 0.0262 x 10-7		
ī	I _r x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'r×10	$7(amps)(I'_T/I'_i)x$	107
20° 30° 40° 50° 60° 70° 80° 20°	0.0573 0.0542 0.0501 0.0460 0.0403 0.0352 0.0294	4.98 5.00 5.01 5.01 5.01 5.01 4.99	2.45 2.42 2.42 2.42 2.42 2.41 2.41	0.03 0.02 0.02 0.01 0.01 0.00	78 6.29 31 5.23 91 4.32 35 3.05 86 1.95	

Record Number 19
O f(r) Measured

 $X \longrightarrow X$ $f(r) = \cos r$



41 9 1 4

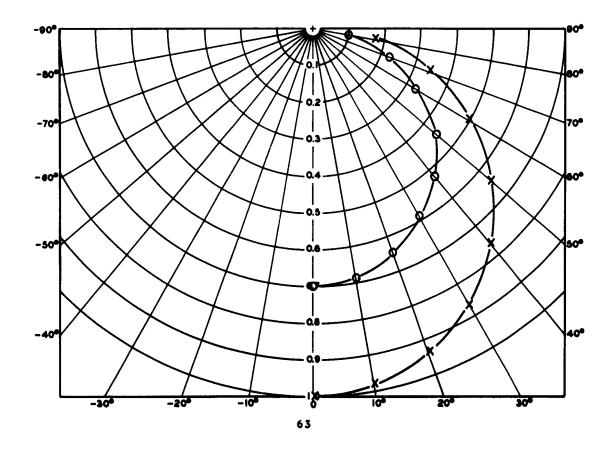
Contract AF 33(657)-9014

Type Remark Incide	ent Light Ref. for Ii		Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	Dis MgC	f. #656 red ffuse Standard sc. 2r=2.5cm) #3. t=2mm i=0°. r=45°
r	(_T x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107(am	ps) (I' _T /I' _j)x10 ⁷
0° 10° 20° 30° 40° 50° 60° 70° 80°	0.0520 0.0514 0.0499 0.0474 0.0450 0.0419 0.0375 0.0337 0.0291	4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.98	2.38 2.38 2.38 2.38 2.38 2.38 2.38 2.38	0.0268 0.0263 0.0248 0.0225 0.0200 0.0171 0.0125 0.0086 0.0038	7.01 6.88 6.49 5.89 5.23 4.48 3.27 2.25 0.99

.1

Record Number 20
O-O f(r) Measured

X----X f(r) = cos r



Contract AF 33(657)-9014

	d number Reflection	21 Diffuse	Incidence Filter Sample Dimensions Coating		i=60° O.T. #656 red Diffuse Standard Disc. 2r=2.5cm MgO #3. t=2mm
Adj.	ent Light Ref. for I _i dj. for ref.]	1;=0.00230 1.66 x 10 ⁻⁷ 0.00243	Reference: For reflected Filter b.c. Lamp I'r adj.	light	at i=0° r=45° I==0.0535 x 10-7 0.T. #656 red 2.70 x 10-9 5.00 volts 0.0271 x 10-7
r	I _r x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107	$(amps) (I'_T/I'_i) \times 10^7$
-20° -10° 0° 10° 20° 30° 40° 50° 60° 70° 80° -20°	0.0437 0.0440 0.0440 0.0438 0.0430 0.0421 0.0410 0.0393 0.0373 0.0350 0.0319 0.0439	5.00 4.99 4.98 4.98 4.98 5.00 5.00 4.99 4.99 5.00 4.99	2.69 2.69 2.70 2.70 2.70 2.70 2.70 2.70 2.70 2.70	0.015 0.015 0.014 0.013 0.012 0.010 0.008 0.005 0.002	5 6.38 8 6.09 2 5.43 0 4.94 8 4.44 7 3.58 5 2.26

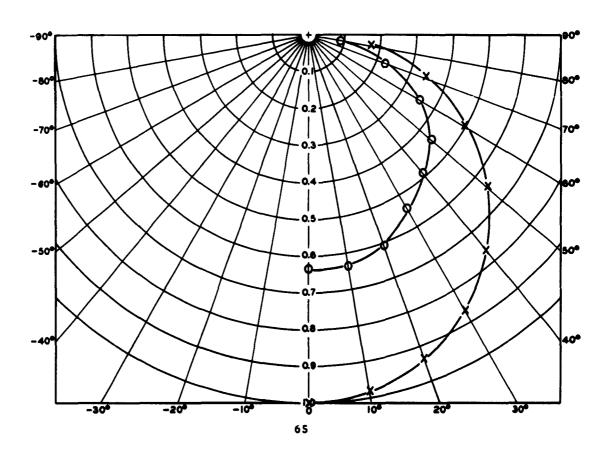
. 1

Function of the Angle of Reflection $f(r)=(I'_r/I'_1) \times 10^7$

Record Number 21

O f(r) Measured

 $X \longrightarrow X$ $f(r) = \cos r$



Record number 22 Type Reflection Remarks: Diffuse Incident Light Adj. Ref. for Ii I' (adj. for ref.) Ii=0.0008 1.66 x 10-7 0.000856			Incidence Filter Sample Dimensions Coating	Diffu: Disc.	656 red se Standard 2r=2.5cm 5. t=2mm
		Reference: For reflected Filter b.c. Lamp I'r adj.	1ight Tr=0.0 0.T. 1 2.67 4.99	at i=0°, r=45° Ir=0,0530 x 10-7 0.T. #656 red 2.67 x 10-9 4.99 volts 0,0274 x 10-7	
r	I _T X10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx10 ⁷ (amps)	(I' _r /I' _i)x10 ⁷
-40 ° 0 ° 40 °	0.0317 0.0322 0.0317	5.00 4.99 4.99	2.70 2.70 2.70	0.0048 0.0056 0.0051	5.60 6.54 5.96

Function of the Angle of Reflection $f(r)=(I'_r/I'_i) \times 10^7$

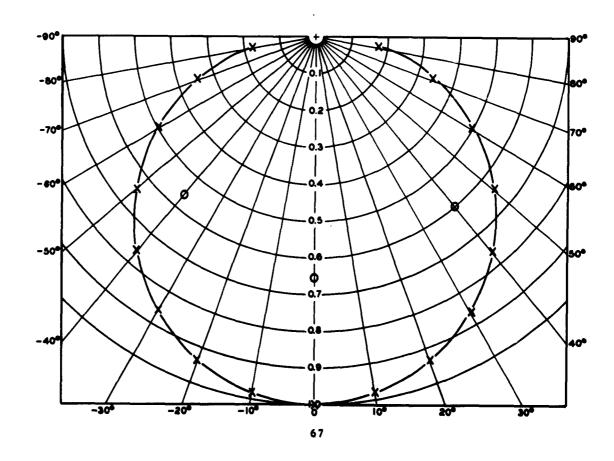
Record Number 22

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f(r) Measured

x----x

 $f(r) = \cos r$



Record number 23 Type Reflection Diffuse-Specular Remarks: Paint coat one day old		Incidence Filter Sample Dimensions Coating			nolished Al 2r=2.5cm Paint	
Adj.	dent Light Ref, for Ii adj. for ref.	0.298 1.66 x 10 ⁻⁷ 0.274	Reference: For reflected Filter b.c. Lamp I'r adj.	light	at i=0 1.44 x None 1.74 x 5.00 y	10-9
r	I_x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'r×10	⁷ (amps)	(I' _r /I' _i)x10 ⁷
35° 40° 50° 60° 70° 80° 85° 35°	1.73 1.60 1.31 1.01 0.645 0.258 0.100 1.71	5.00 5.00 5.00 5.00 5.00 4.99 4.99	1.54 1.54 1.54 1.54 1.62 1.62	1.67 1.54 1.26 0.96 0.61 0.23 0.08	6 0 9	

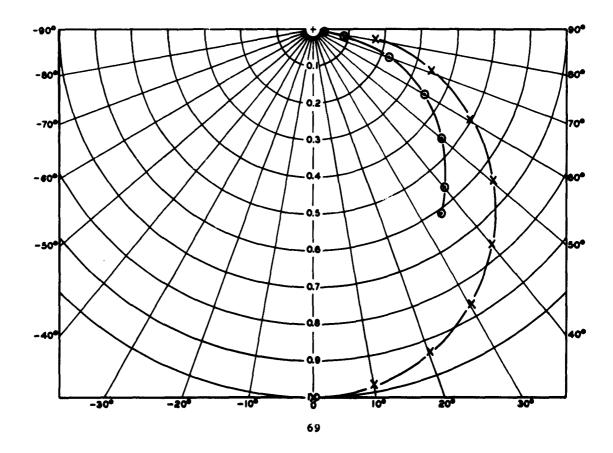
Function of the Angle of Reflection $f(r)=(I'_r/I'_i) \times 10^7$

Record Number 23

f(r) Measured

x----x

 $f(r) = \cos r$



Type Re Remarks compar Incider Adj. Re	number iflection i: Refs. fo ed to full it Light if. for Ii j. for ref.	0.298 cos 45° 1.66 x 10 ⁻⁷	Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	Dis Whit light 1.4 Non- 2.1 5.0	on polished A1 c, 2r=2.5cm te Paint i=0°, r=45° 2 x 10-7
r I,	x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'_x107(amp	s) (I' _T /I' ₁)x10 ⁷
-10°	1.43	4.98	2.13		
0.	1.42	4.99	2.13	1.39	7.29
10°	1.39	4.99	2.13	1.35	7.08
20°	1.33	4.99	2.13	1.29	6.77
30°	1.25	4.98	2.14	1.21	6.35
40°	1.64	4.98	2.14	1.61	8.44
50°	1.79	4.98	2.13	1.76	9.23
60 °	0.721	4.98	2.13	0.711	3.73
70 °	0.450	4.98	2.13	0.435	2.28
80°	0.193	4.98	2.15	0.173	0.907
85 °	0.083	4.98	2,15	0.060	0.315
-10°	1.39	4.98	2,15		
45* *	2.18	4.98	2.21	2.15	1130.

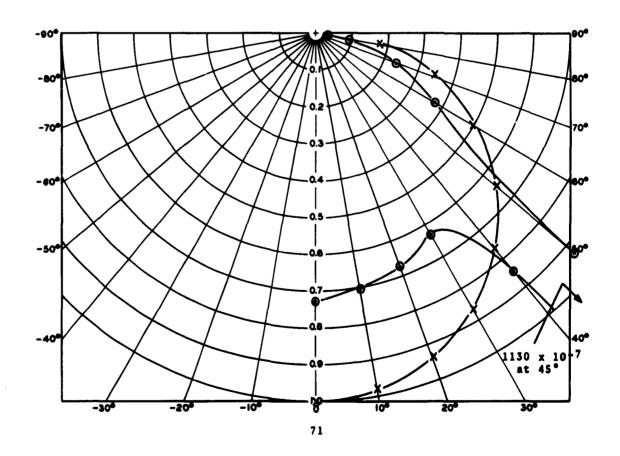
^{*} N.D. #2

Function of the Angle of Reflection $f(r)=(I'_r/I'_i) \times 10^7$

Record Number 24

⊙—⊙ f(r) Measured

X----X f(r) = cos r



Contract AF 33(657)-9014

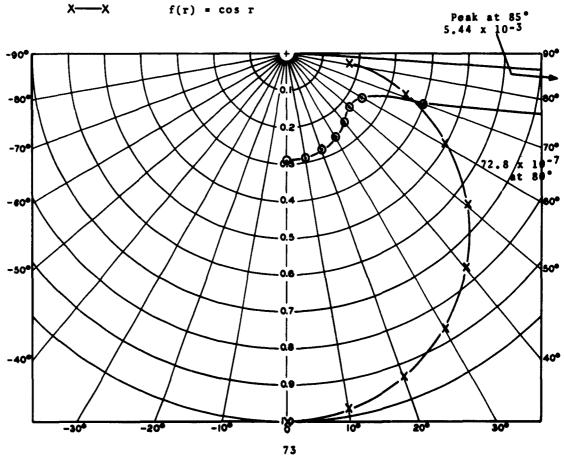
Type Remarkis 0. Incidadj.	d number Reflection ks: Sample v 115 or 1,15 ent Light Ref. for Ii dj. for ref.	Diffuse-Specular ery flat. I. at 70° 0.298 cos 85° 1.66 x 10-7 0.0228 except at i=r	Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	Disc. White at i: 1.38 None 2.16 5.00	on polished Al 2r=2.5cm Paint Paint 10-7 volts x 10-7
r	I _r x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107(amps	$(1'_{T}/1'_{i}) \times 10^{7}$
o •	0.0880	4.99	2.15	0.0664	2.91
10°	0.0872	4.99	2.15	0.0657	2.88
20°	0.0850	4.99	2.15	0.0635	2.79
30°	0.0815	4.99	2.15	0.0602	2.64
40°	0.0770	4.98	2.15	0.0553	2.43
50°	0.0735	4.98	2.15	0.0513	2.25
60°	0.0770	4.98	2.15	0.0543	2.38
70°	0.115	4.98	2.15	0.091	3.99
80°	1.70	4.98	2.15	1.66	72.8
0.	0.0880	4.98	2.17	0.0664	2.91
85 *	12.5	4.98	2.21	12.4	54,400.

* N.D. #2

Function of the Angle of Reflection $f(r)=(I_r'/I_1') \times 10^7$

Record Number 25

f(r) Measured



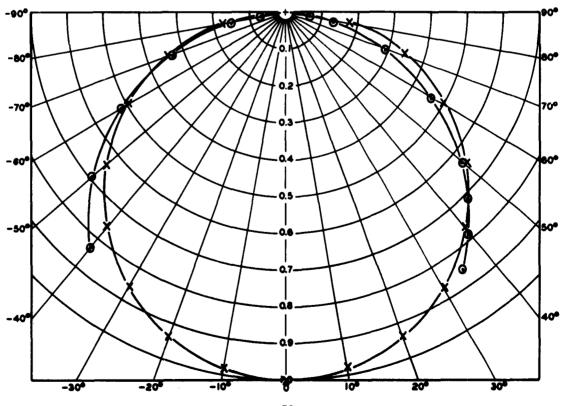
Record number Type Reflection Remarks: Not norms subtracted. Incident Light Adj. Ref. for Ii I'i (adj. for ref.)	No. ref.	Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	light	2.8 x	bluc surface mirror 1.7=4,76cm ² , t=0.5mm
r I _r x10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'r×107	(amps)	(I' _T /I' ₁)x10 ⁷
35° 0.87	5.0	2.00	0.85		
40° 0.80	5.0	2.00	0.78		
45° 0.73	5.0	2.00	0.71		
50 0.65	5.0	2.00	0.63		
60° 0.48	5.0	2.00	0.46		
70° 0.31	5.0	2.00	0.29		
80 0.15	5.0	2.00	0.13	-	
85° 0.085	5.0	2.00	0.06	5	
-40° 0.85 -50° 0.71	5.0	1.87	0.83		
-50° 0.71 -60° 0.54	5.0 5.0	1.85 1.85	0.69		
-70° 0.35	5.0	1.83	0.32		
-80° 0.17	=	-	0.33		
-85° 0.087	5.0	1.83			

Function of the Angle of Reflection $f(r) = (I'_r/I'_i) \times 10^7$

Record Number 29

⊙—⊙ f(r) Measured

 $X \longrightarrow X$ $f(r) = \cos r$



Contract AF 33(657)-9014

Type Remai subt	rd number Reflection rks: Not norm racted dent Light Ref. for Ii adj. for ref.	30 Diffuse salized only d.c. No ref.	Incidence Filter Sample Dimensions Coating Reference: For reflected Filter b.c. Lamp I'r adj.	light	i=20° Wr #47 Front surface mirror 2.8 x 1.7=4.76cm ² MgO #1, t=0.5mm
r	I _T x10 ⁷ (amps)	Lamp Voltage(volt	s) b.c.x109(amps)	I'r×10	$^{7}(amps) (I'_{T}/I'_{i}) \times 10^{7}$
15° 20° 25° 30° 40° 50° 60° 70° 80° 85°	1.02 1.08 0.93 0.88 0.76 0.63 0.48 0.32 0.16 0.085	5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0	1.77 1.77 1.77 1.75 1.75 1.75 1.75 1.75	1.00 1.06 0.91 0.86 0.74 0.61 0.46 0.30 0.14	

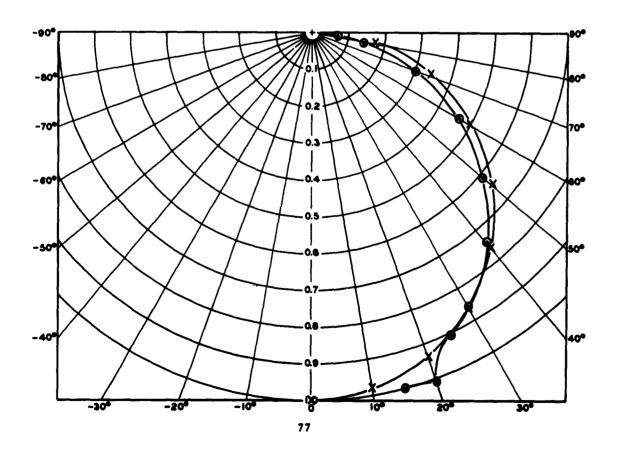
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Function of the Angle of Reflection $f(r) = (I'_r/I'_i) \times 10^7$

Record Number 30

0-0 f(r) Measured

 $f(r) = \cos r$



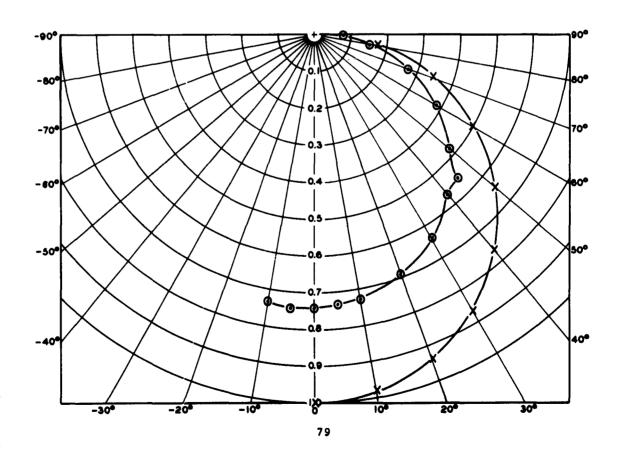
Record number 31 Type Reflection Diffuse Remarks: Not normalized, only d.c. subtracted		Incidence Filter Sample Dimensions Coating		i=45° Nr #47 blue Front surface mirro 2.8 x 1.7=4.76cm ² MgO #1, t=0.5mm	
Adj. i	ent Light Ref. for I _i dj. for ref		Reference: For reflected Filter b.c. Lamp I'r adj.	light	None
r	I _r x10 ⁷ (amps) Lamp Voltage (vo	lts) b.c.x109(amps)	I'rx10	(amps) (I'r/I'jx10 ⁷
-10°	0.755	5.0	1.90	0.73	
-5	0.765	5.0	1.95	0.74	
0° 5°	0.765	5.0	1.95	0.74	
	0.755	5.0	2.00	0.73	
10° 20°	0.750 0.710	5.0	2.00 2.00	0.73	
30°		5.0	2.08	0.69	
40°	0.660 0.585	5.0 5.0	2.08	0.63	
45	0.572	5.0	2.08	0.55	
50°	0.502	5.0	2.14	0.33	
60°	0.405	5.0	2.14	0.38	
70°	0.403	5.0	2.15	0.36	
80*	0.168	5.0	2.15	0.14	
85*	0.098	5.0	2.15	0.07	

Function of the Angle of Reflection $f(r)=(I'_r/I'_1) \times 10^7$

Record Number 31

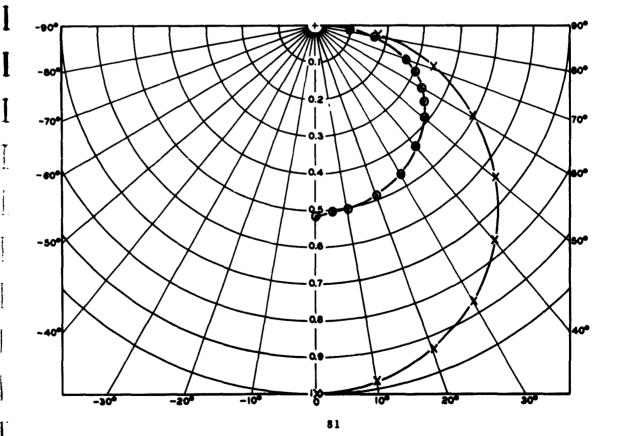
⊙—⊙ f(r) Measured

 $X \longrightarrow X$ $f(r) = \cos r$



Record number 32' Type Reflection Diffuse Remarks: Not normalized, only d.c. subtracted		Incidence Filter Sample Dimensions Coating		i=60° Wr #47 blue Front surface mirro 2.8 x 1.7=4.76cm ² MgO #1, t=0.5mm	
Adj.	ent Light Ref. for Ii dj. for ref.)	No ref.	Reference: For reflected Filter b.c. Lamp I'r adj.	light	None
r	I _x x10 ⁷ (amps)	Lamp Voltage (volts)	b.c.x109(amps)	I'r×10	7(amps) (I' _T /I' _j)x10 ⁷
0* +5* 10* 20* 30* 40* 50* 65* 60* 65* 70* 80*	.535 .530 .528 .510 .485 .448 .407 .381 .358 .321 .283 .183	5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0	2.00 2.05 2.10 2.10 2.10 2.06 2.06 2.06 2.06 2.06 2.06 2.03 2.03	0.51 0.50 0.50 0.48 0.46 0.42 0.38 0.36 0.33 0.26 0.16	9 7 9 4 7 6 6 0 7 0 3

Function of the Angle of Reflection $f(r)=(I'_r/I'_1) \times 10^7$



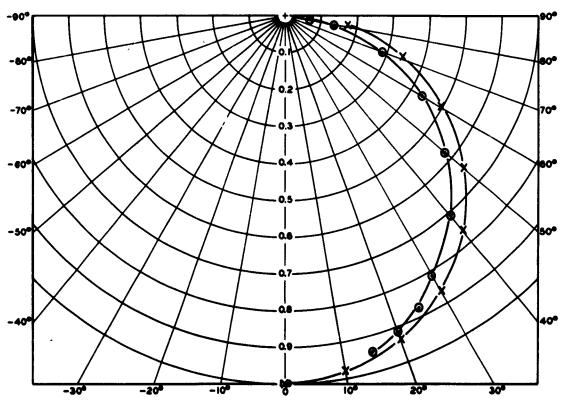
Record number 33 Type Reflection Diffuse Remarks: Not normalized, only d.c. subtracted Incident Light No ref. Adj. Ref. for Ii I'i (adj. for ref.)		Incidence Filter Sample Dimensions Coating		i=20° Wr #47 blue Front surface mirror 2.8 x 1.7=4.76cm ² MgO #2. t=1mm	
		Reference: For reflected light Filter b.c. Lamp I'r adj.		None	
r	I _r x10 ⁷ (amps)	Lamp Voltage(volts	b.c.x109(amps)	I'r×107	(amps) (I'r/I'jx107
15° 20° 25° 30° 40° 50° 60° 70° 80° 85°	0.970 0.940 0.900 0.840 0.735 0.600 0.458 0.308 0.161	5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0	2.53 2.53 2.53 2.53 2.53 2.53 2.53 2.53	0.94 0.91 0.87 0.81 0.71 0.57 0.43 0.28	5 5 5 0 5 3 3 6

Function of the Angle of Reflection $f(r)=(I_r'/I_1') \times 10^7$

Record Number 33

⊙——**⊙** f(r) Measured

 $X \longrightarrow X$ $f(r) = \cos r$



Record number 26 Type Reflection Diffuse-Specular Remarks: Full beam ref. for I; meas. = 3.96 x 10-7		Incidence Filter Sample Dimensions Coating		ND #2 W.P. on polished A Disc. 2r=2.5cm White Paint		
Adj. R	ef. for Ii	0.298 (cos i) 1.66 x 10 ⁻⁷ 0.00268 (cos i)	Reference: For reflected Filter b.c. Lamp I'r adj.	light	At i=0° x=45° 1.37 x 10-7 None 2.18 x 10-9 4.98 volts 1.35 x 10-7	
r I	rx10 ⁷ (amps) La	mp Voltage (volts)	b.c.x109(amps)	I'rx10	(amps) (I' _T /I' ₁)x10 ⁷	
60° 17.5°	3.97 1.50	4.98 4.98	2.20 2.20	3.93 1.46	2930. 570.	
Refere	nce: full bear	n with filters ND	#2, #3, #1			
180 *	3.60	4.98	2.19	3,56		

Type R Remark			Incidence Filter Sample Dimensions Coating	Disc.	n polished AL 2r=2.5cm Paint
Adj. R	nt Light ef. for Ii j. for ref.)	0.298 cos i 1.66 x 10-7 0.00384 (cos i)	Reference: For reflected Filter b.c. Lamp I'r adj.	1ight 5.25 ND #2 2.35 5.00	*3. #1 * 10-7
rI	rx10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'x107(amps) (I' _T /I' _j)x10 ⁷
17.5° 45°	1.30 1.54	4.99 4.99 4.99	2.35 2.35 2.35	1.25 1.48 7.85	342. 546. 23.500.

Type R	number eflection s: <u>High pol</u>		Incidence Filter Sample y Dimensions Coating	Polis	. ND #1 hed A1 2r=2.5cm
Adj. R	nt Light ef. for I _i j. for ref.)	0.298 (cos i) 1.66 x 10-7 3 x 10-5 (cos i)	Reference: For reflected Filter b.c. Lamp I'r adj.	ND #2 2.37 4.98	beam at 180° x 10-7 x 10-9 x 10-9 volts x 10-7
r I	rx10 ⁷ (amps)	Lamp Voltage(volts)	b.c.x109(amps)	I'rx107 (amps)	[I'r/I'sk107
17.5° 45° 60° 85°	0.189 0.135 0.108 0.0514	4.99 4.98 4.98 4.98	2.33 2.34 2.35 2.35	0.165 0.111 0.084 0.0244	5770. 5240. 5600 •

^{*} Error in B.G. off shaft